

## LP-SW902FGP

9 port Midspan PoE Ethernet Switch with 8x10/100M PoE ports plus 1x10/100/1000M copper port interchangeable with 1x SFP Gigabit port. Power Over Ethernet output specifications test.

The purpose of this test is to stress the device near its maximum values at an ambient temperature of approximately $24^{\circ} \mathrm{C}$ during two sessions of 9 hours each.

At the same time, the hottest temperature will be observed on the PoE Output driver circuitry heat sink to see if it exceeds expected values.

Tests will be performed at low AC input line voltage near 100 VAC. This will stress the power supply because current will rise to maintain the power output.

All outputs will be loaded so as to be near the 112 W maximum Power specified at room temperature.

## Bench Test Setup

The test setup shown in Figure 1 includes the following parts:

| a.- | One (1) Current and Over-Voltage Protected Power <br> Distribution Unit Model LP-RU07107PPDU. |
| :--- | :--- |
| b.- | One (1) B\&K Precision Model 1653A Isolation Transformer <br> and Variac. |
| c.- | One (1) Cable fixture for Line Voltage and Input current <br> measurement. |
| d.- | One (1) Power Clamp B\&K Precision Model 5330A. |
| e.- | One (1) Dual K-Type Thermometer B\&K Precision Model <br> 630. |
| f.- | One (1) LanPro LP-SW902FGP PoE Switch. |
| g.- | Eight 0.5 m LanPro CAT 5e Patch Cords. |
| h.- | Eight (8) LP-PoE151 802.3af PoE splitters with the output <br> set to 12VDC. |
| i.- | Eight (8) PoE Splitter cables for connection to Resistor <br> Loads. |
| j.- | One (1) 24 Port Resistive Load. |
| k.- | One (1) test fixture for measuring Ethernet port PoE <br> current and voltage output. |
| I.- | Two (2) B\&K Precision Model 390A Multimeters with Test <br> Leads. |
| m.- | One LP-PoE151 PoE Splitter output current and voltage <br> measurement cable and terminal test fixture. |



Figure 1


## C Sequence of Testing

## 1 Initial Ambient temperature

One of the thermocouple input sensors is measuring free air temperature around the setup for comparisons purposes, Tamb $=23.6^{\circ} \mathrm{C}$ as shown in Figure 2.


Figure 2

## 3 Power line Voltage

We need to test the LP-SW902FGP with a low line voltage of about 100 VAC, larger than the $-10 \%$ expected low. Actually, we assume a $16.25 \%$ less than the nominal 120 VAC for this test. Our measurement with the Power Meter is Vin: 100.5 VAC as shown in Figure 4.


Figure 4. Input AC Voltage measured: 100.5 VAC

## 2 Input Voltage adjustment

For the adjustment of the input voltage, we have selected a Variac Auto-Transformer with an internal isolation transformer model 1653A by B\&K Precision with a maximum current of 2 Ampere AC.


Figure 3

## 4 Power Line current

The Line current is measured giving a Figure of 1.6 A for the loading conditions specified above, please see Figure 5.


Figure 5. Line Current Amperes read: 1.6 Ampere AC

5 Real Power Measurement

The measured Real Power is 130 Watt as shown in Figure 6.


Figure 6. Real Power=0.13 (KWatt)

7 Power Factor measurement
The power factor measured is: 0.8 .


Figure 8. Power Factor=0.8

## 6 Apparent Power (Volt-Ampere)

The measured Apparent Power is 0.17 (KVA).


Figure 7. Apparent Power measurement is 0.17 KVA

## 8 Temperature difference between Tamb and Tair

A temperature Differential, Tdiff, between the ambient temperature and the air expelled by the Switch fans in the rear of the DUT stabilized around 9.7 degrees Centigrade and was measured after 4 hours.


Figure 9. Temperature differential after 4 hours $=9.7^{\circ} \mathrm{C}$

## 9 LP-SW902FGP Switch front view showing led indications

The first Row of the Switch from top to bottom called PoE shows a Red Led ON indication when the port is connected to a IEEE 802.3af compatible load and is active as a PoE source.


Figure 10. Showing Led Indications

11
PoE Splitters connections for powering the resistive load.

Each port is loaded with a LP-PoE151 IEEE 802.3af splitter that feed a Resistor load.

Their output has been selected with a sliding switch to be 12 VDC. The Figure 12 shows the eight (8) splitters simultaneously connected to the resistive load.


Figure 12. PoE Splitters loading the switch

## 10 Measurement of PoE Port voltage and current

A fixture for connecting Multimeter inputs to one of the ports was necessary, a current of 0.31 Ampere and a voltage of 46.6 DC Volt was measured. A calculation of DC power gives a value of 14.4460 Watt exiting the port.

The sum of all the ports loaded in the same manner gives a value of $14.4460 \times 8=115.57$ Watt, producing an overload of 3,57 Watt over the 112 Watt shown in the specifications. This produces some stress (3.19\%) on the power supply forcing an extreme condition on the Test.


Figure 11. PoE port values

## 12 Resistive load

A FAN cooled resistive load was assembled with a typical value of 11.69 Ohm per circuit when hot.


Figure 13. Resistive Load

The splitter output was measured and gave a typical value for one port of 11.74 VDC and 1.09 ADC, a DC Power of 12.79 W results.


Figure 14. Load measurements

## 14 Power Supply temperature

Temperature of the power supply was measured after several hours of operation and was $56.3^{\circ} \mathrm{C}$.


Figure 15

15 Results

| AC input | Active Power AC (W) | 130 |
| :---: | :---: | :---: |
|  | Apparent Power AC (VA) | 170 |
|  | Power factor AC (PF) | 0.8 |
|  | Input Voltage AC (V) | 100.5 |
|  | Current Input (A) | 1.6 |
| Ethernet-PoE port | $\mathrm{V}_{\text {poe }}$ Output Voltage DC (V) | 46.6 |
|  | $\mathrm{I}_{\text {poe }}$ Output Current DC (A) | 0.31 |
|  | $\mathrm{P}_{\text {poe }}$ DC Power (W) | 14.4460 |
| Splitter output to RL | Output Voltage DC (V) | 11.74 |
|  | Output Current DC (A) | 1.09 |
|  | DC Power (W) | 12.79 |
| Ethernet-PoE ports output power sum | $8 \times\left(\mathrm{P}_{\mathrm{poe}}\right)(\mathrm{W})$ | 115.57 |
| Temperature difference | 4 hours ( ${ }^{\circ} \mathrm{C}$ ) | 9.7 |
| Power Supply Temperatur | Tps ( ${ }^{\circ} \mathrm{C}$ ) | 56.3 |
| PoE Part Heat Sink Maximun Temperature | $\left({ }^{\circ} \mathrm{C}\right)$ | 70.0 |

## 16 <br> Conclusions

After this test we arrived to the following conclusions that can guide the user on how to safely operate the LP-SW902FGP.

The Switch performs inside design constraints and without elevated temperatures. The power supply is properly under-rated for operation at temperatures over $30^{\circ} \mathrm{C}$.

Warning: You shall not surpass the design limit of 112 W at ambient temperature, it shall be de-rated linearly as shown in the following paragraphs in order to avoid lowering the reliability or cause over heating and damage.

## Safe loading

Even though the Power Supply maximum rating is 200 W , the sum of all ports shall not exceed the 112 W maximum rating at a $24^{\circ} \mathrm{C}$ Tamb due to PoE port limitations. This is so in order to keep the Switch inside the safety operating area.

If you plan to operate this switch above $30^{\circ} \mathrm{C}$ of ambient temperature, please derate linearly to 0 Watt @ $40^{\circ} \mathrm{C}$.

## Example: Ambient temperature of operation: $35^{\circ} \mathrm{C}$

Before loading the switch ports with PoE compatible devices, calculate the sum of all the maximum loads applied to the switch outputs considering they are IEEE 802.3af compatible devices.

| Pmax $=-11.2 x\left(\mathrm{~T}_{\text {oper }}-30\right)+448[\mathrm{~W}]$ |
| :---: |
| $\operatorname{Pmax}=-11.2 \times(35-30)+448[\mathrm{~W}]$ |
| $\operatorname{Pmax}=56.0[\mathrm{~W}]$ |

At $35^{\circ} \mathrm{C}$ of ambient temperature you shall not load the switch with more than 92.2 Watt for the sum of all the outputs.

A maximum load per circuit shall be then: 7.0 W @ up to $35^{\circ} \mathrm{C}$ at each output port of the switch but you must take into consideration the DC resistance of the Cable to the Powered Device (PD), this will further reduce the available power to this remote device at the end of the cable path.

At $20^{\circ} \mathrm{C}$ you could expect the values shown in Figure 16.


If the cabling temperatures reaches e.g.: $45^{\circ} \mathrm{C}$, a derating for the cable also happens because resistance augments with temperature a rate of $+0.4 \% /{ }^{\circ} \mathrm{C}$, causing the original 9.38 Ohm to become more resistive in an amount proportional to the temperature difference respect to $20^{\circ} \mathrm{C}=$ $45^{\circ} \mathrm{C}-20^{\circ} \mathrm{C}=25^{\circ} \mathrm{C}$

Figure 16
If we multiply this difference by the rate of increase of resistance $=0.4 \% /{ }^{\circ} \mathrm{C}$ the result is:
$\%$ increase $=24^{\circ} \mathrm{C} \times 0.4 \% /{ }^{\circ} \mathrm{C}=9.6 \%$
Hence the resistance of the cable at $45^{\circ} \mathrm{C}$ is: 9.38 Ohm $\times(1+9.6 \% / 100 \%)=$ resulting: 10.28 Ohm .
The Power loss will then be: $1,058 \mathrm{~W}$ and the maximum power available to the load is: $=7.0 \mathrm{~W}-1.058 \mathrm{~W}=5.9420(\mathrm{~W})$
At this temperature of $45^{\circ} \mathrm{C}$ the powered devices cannot draw more than 5.9420 [W] per port to this type of PoE Switch to operate inside the safety operating area.

